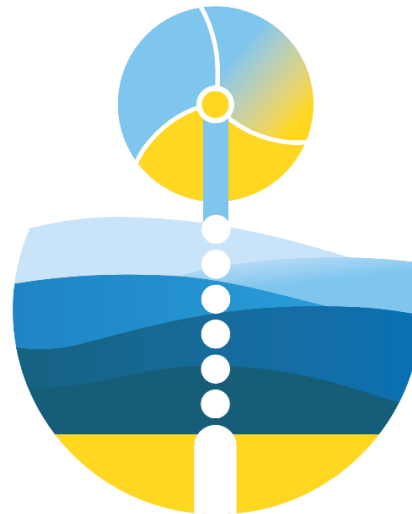


Meta-modelling techniques for the design of offshore anchor piles



SEAFLOWER
for floating wind energy

*This project has received funding from the European Union's
Horizon 2020 research and innovation programme under
Marie Skłodowska-Curie grant agreement number **891826***

23 September 2021



SEAFLOWER

Strategies to Exploit Anchors for Floating Offshore Wind Energy Reaping

MSCA-IF-GF

BENEFICIARY

PARTNER

INSTITUTES



TEAM

Laura Govoni

Christophe Gaudin

Phil Watson

Franck Bourrier

TIMELINE

$t = 3 \text{ years}$

15 March 2021

July 2021

23 Sep 2021

Jan 2023

March 2023

March 2024



3M

18M

3M

12M

SECONDMENT

OUTGOING

SECONDMENT

RETURN



SEAFLOWER

Strategies to Exploit Anchors for Floating Offshore Wind Energy Reaping



MSCA-IF-GF

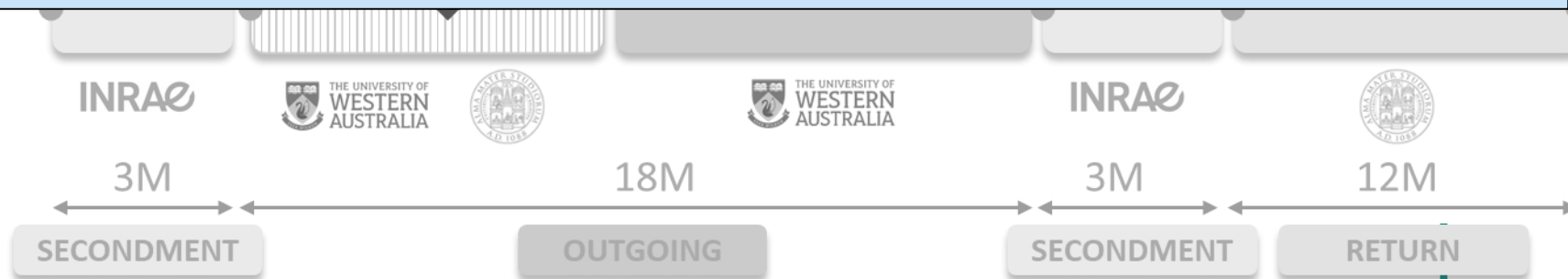
BENEFICIARY

PARTNER

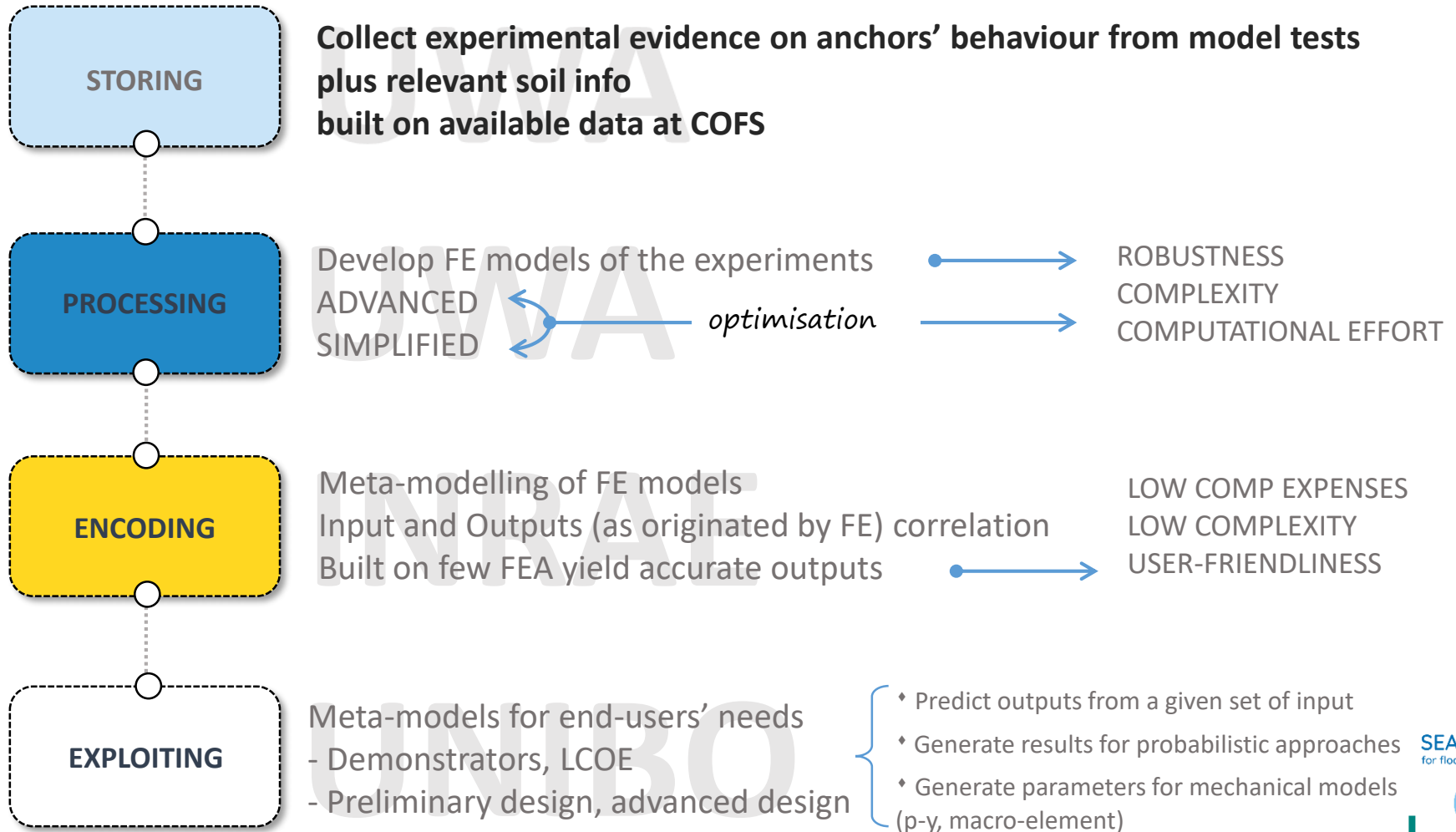
INSTITUTES



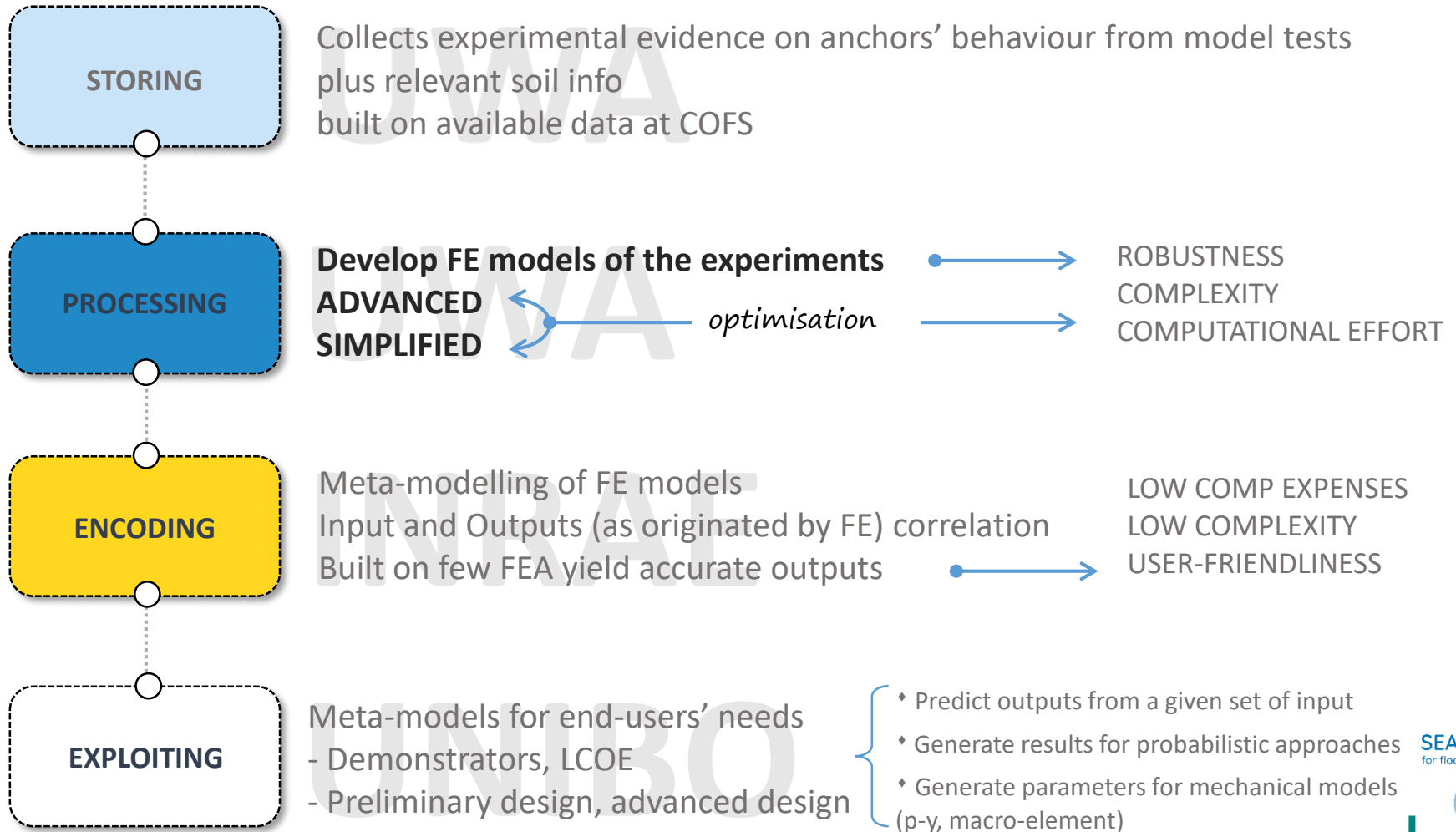
- Support the phase of **pre-commercial** development of floating wind technologies from the **geotechnical standpoint**.
- Aid with a rational **technology transfer** between the **O&G** and **wind market**.
- Develop a procedure to **store previous experience** on anchors and **make it available** for the **new needs of the wind sector**.



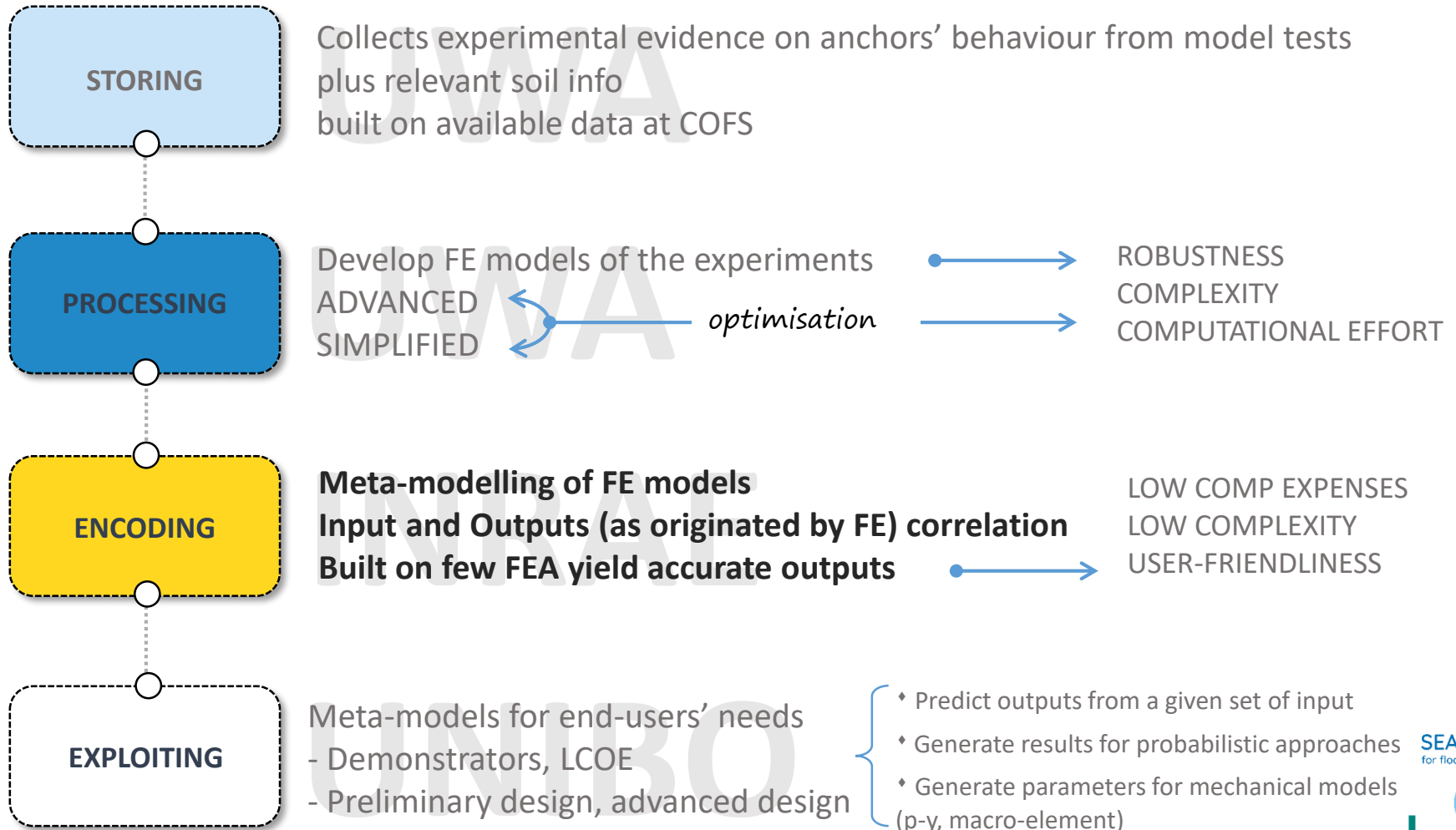
What SEAFLOWER does



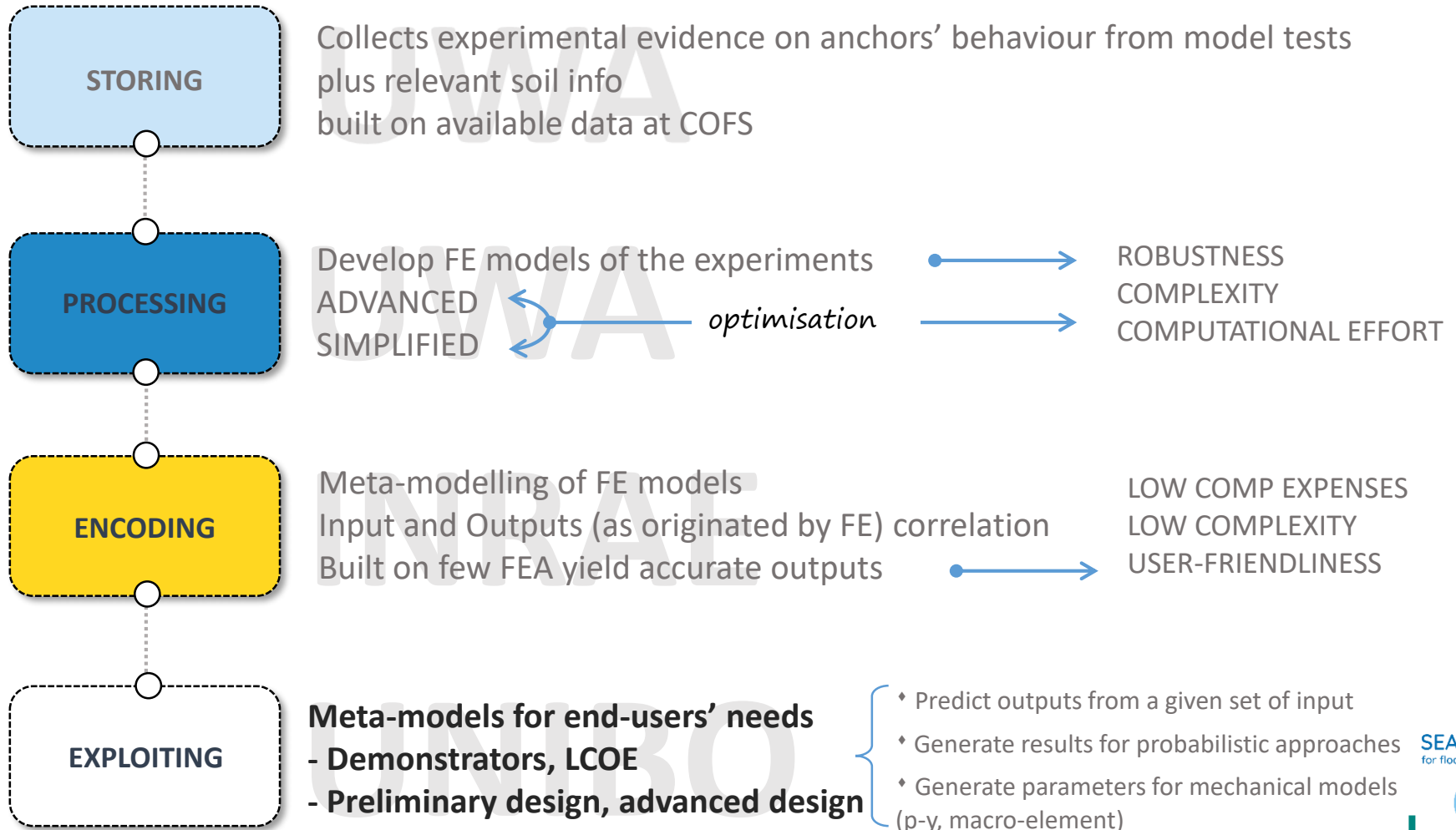
What SEAFLOWER does



What SEAFLOWER does



What SEAFLOWER does



outline

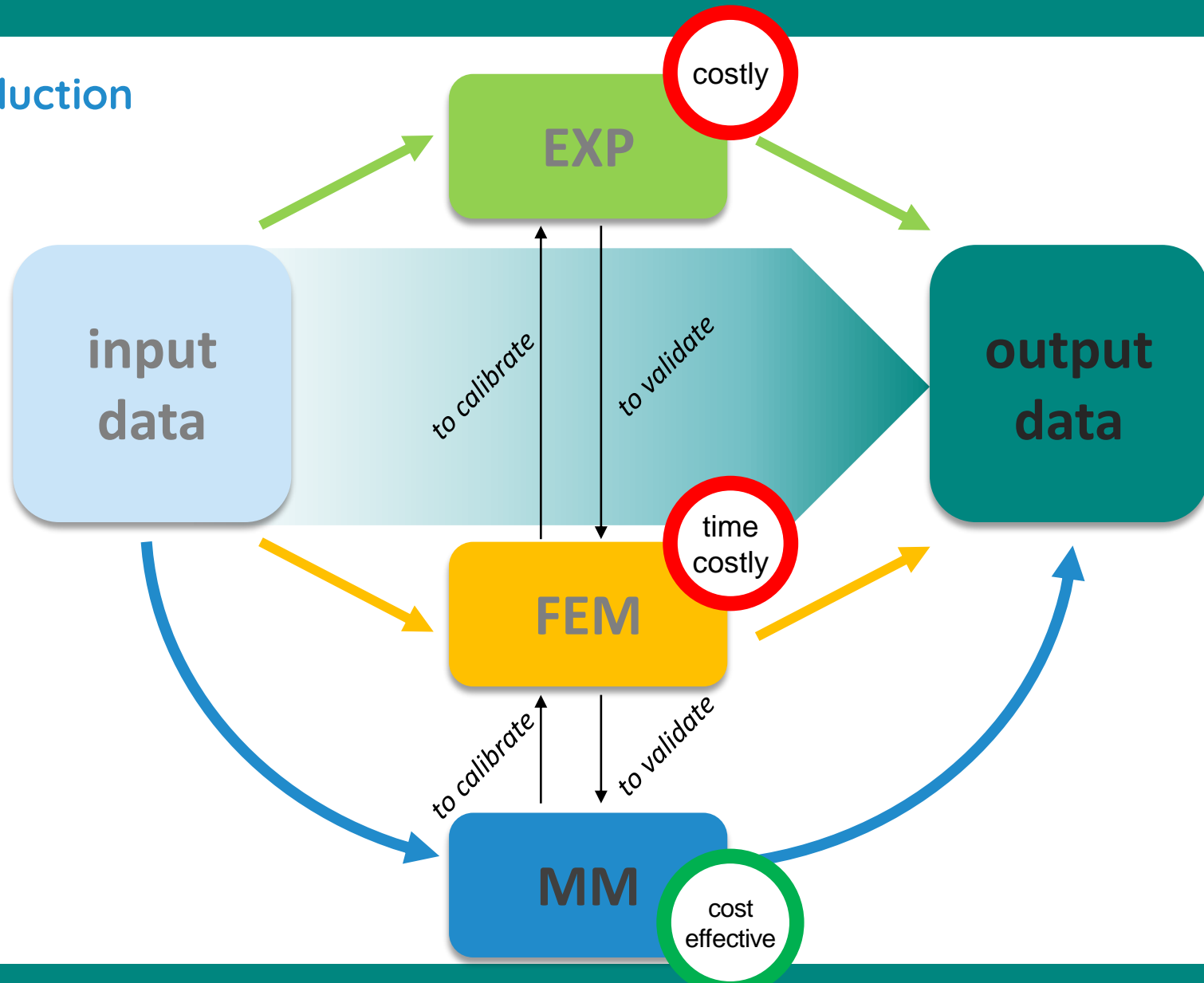
- ❑ Introduction

- ❑ Finite Element Model
 - Details
 - FE testing programme
 - Sampling with LHS
 - Results

- ❑ Metamodelling: the PCE
 - Details
 - Applications and results

- ❑ Conclusions

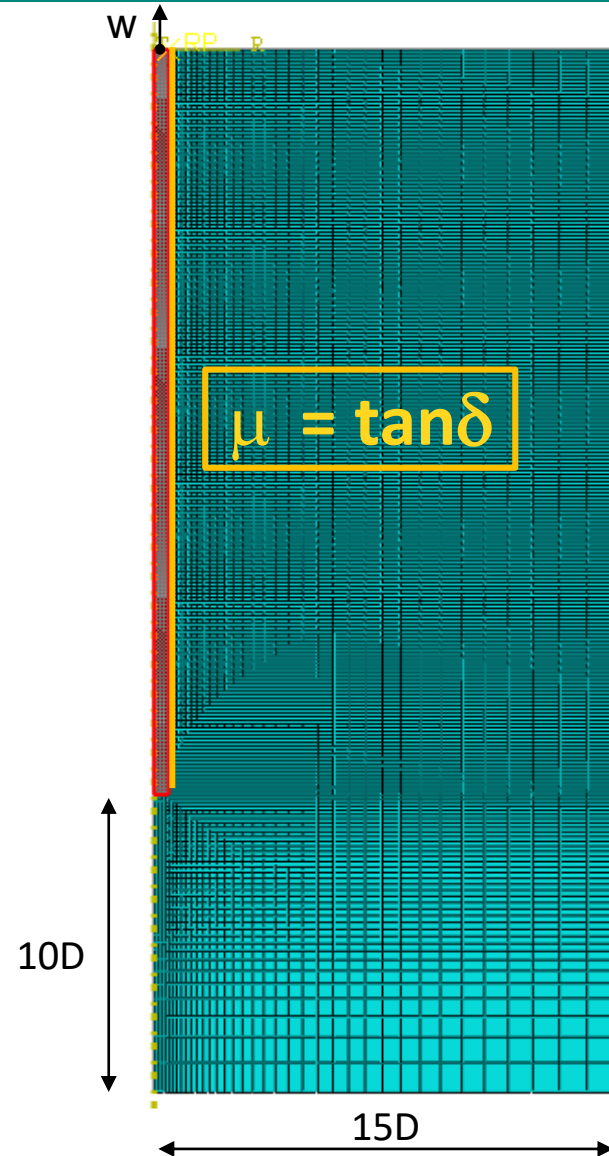
introduction



FEM: details

Proof of concept: anchor pile in sand

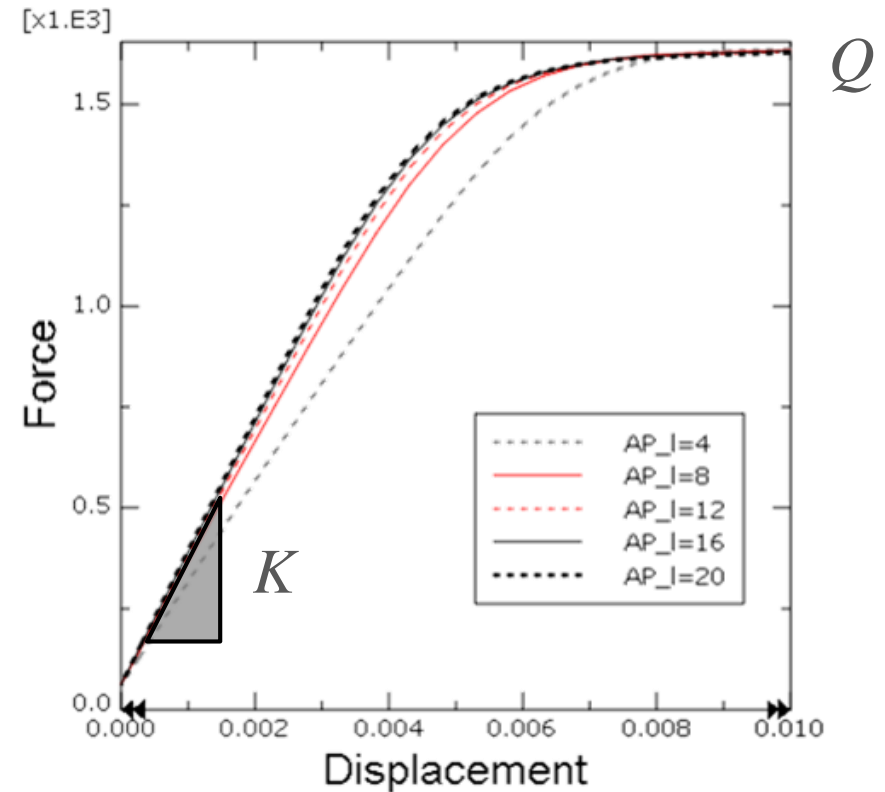
- ❖ Axial-symmetric 2D FEM
- ❖ Soil:
 - homogeneous, $D_r = \text{const}$
 - linear elastic, $E = f(z)$
 - M-C criterion, $\phi', \psi' = f(z)$
- ❖ Pile:
 - linear elastic homogeneous
- ❖ Interface: friction law ($\delta = 29^\circ$)
- ❖ Soil stress state: Jardine et al. 1998
- ❖ Load condition: monotonic tensile ($w = 10\%D$)



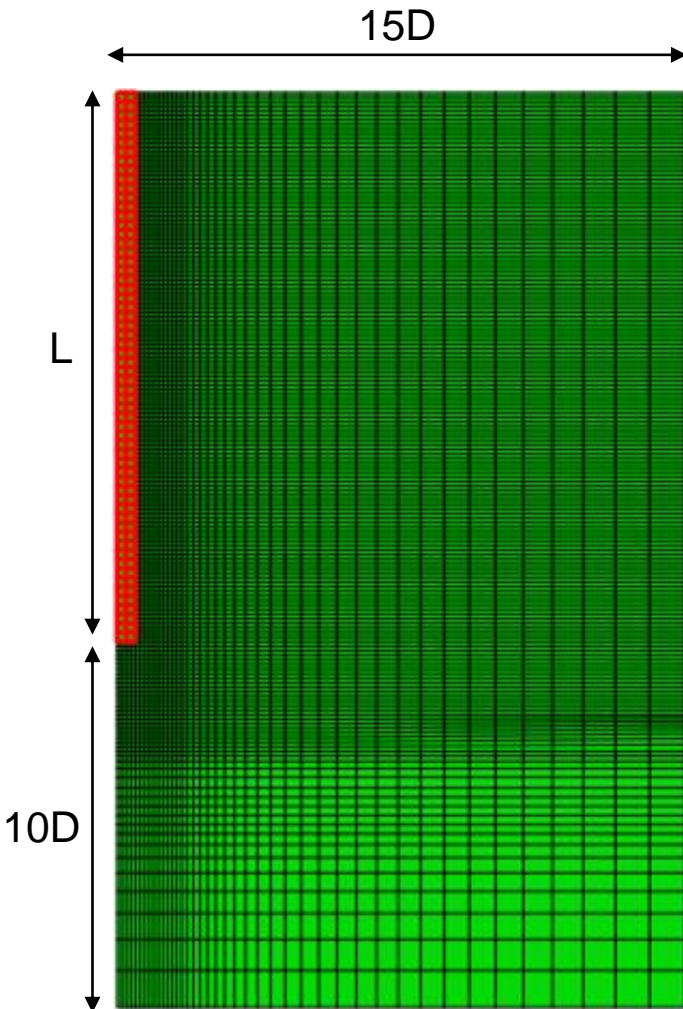
FEM: problem position

FEM input parameters	Symbol [unit]
Pile diameter	D [m]
Pile slenderness	L/D [-]
Wall thickness ratio	D/t [-]
Soil relative density	D_r [%]
Factor for elastic modulus	α [-]

FEM output	Symbol [unit]
Bearing capacity	Q [kN]
Initial stiffness	K [kN/m]



FEM: details



$$q_c = C_0 p_a \left(\frac{\sigma'}{p_a} \right)^{C_1} \exp(C_2 D_R)$$

after Schmertmann, 1976

$$C_0 = 24.94; \quad C_1 = 0.46; \quad C_2 = 2.96$$

after Jamiolkowki et al. 2001

$$C = \alpha q_c$$

$$E' = \frac{(1+\nu)(1-2\nu)}{1-\nu} C$$

$$3 \leq \alpha \leq 9$$

after Baldi et al. 1982

$$\sigma'_{rc} = 0.029 \cdot q_c \left(\sigma'_{v0} / p_a \right)^{0.13} \left(\frac{h}{R^*} \right)^{-0.38}$$

after Jardine et al. 1998

$$I_R = D_r (10 - \ln p'_0)$$

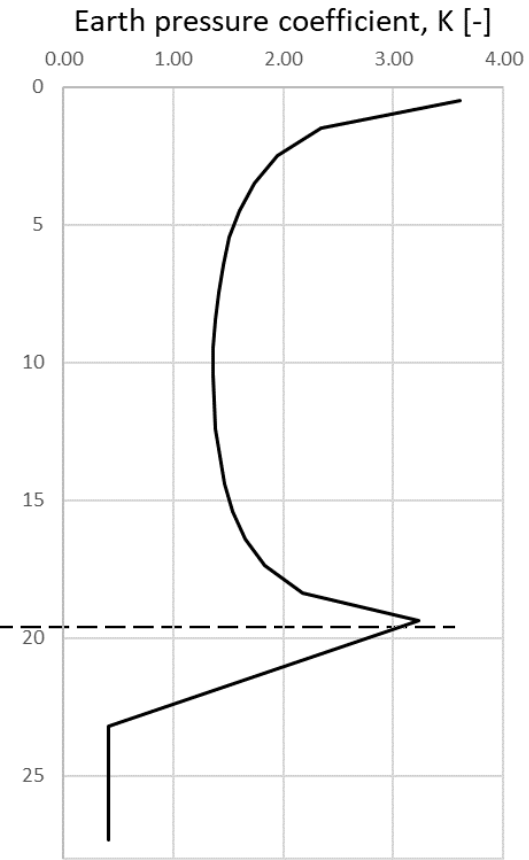
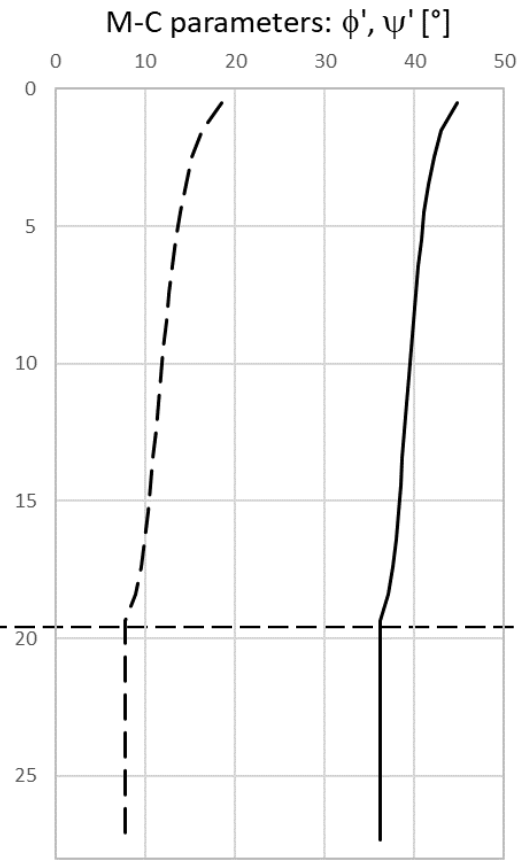
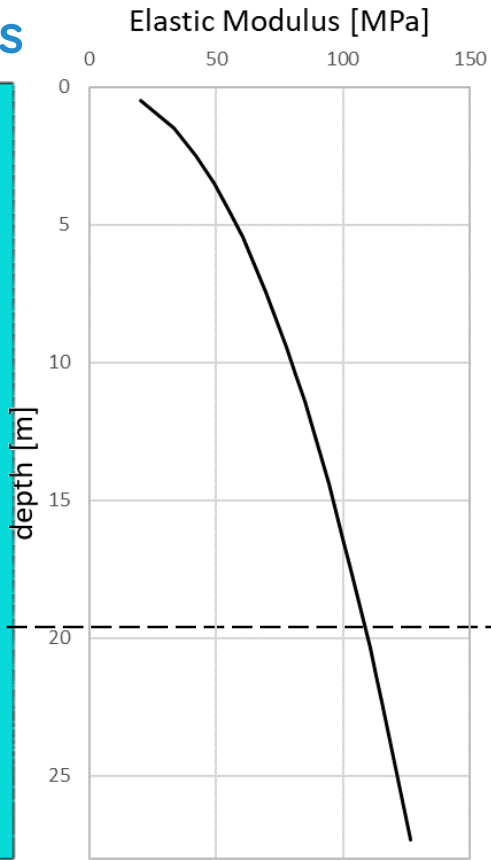
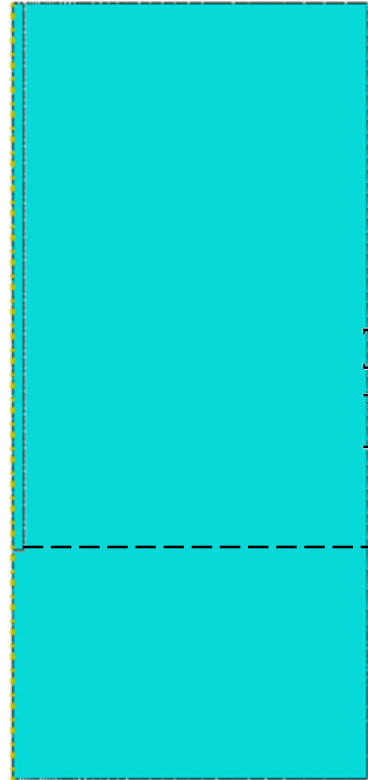
$$3I_R = 0.8\psi'$$

after Bolton, 1986

$$\phi_p = \phi_{cr} + 0.8\psi'$$

input parameters
D [m]
L/D [-]
D/t [-]
D_r [%]
α [-]

FEM: details



input parameters	$D = 0.830\text{m}$	$L/D = 23.925$	$D/t = 25.372$	$D_r = 80.44\%$	$\alpha = 4.797$
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FEM: FE testing programme

A sample of $N=100$ simulations is created by varying the input model parameters within reasonable ranges

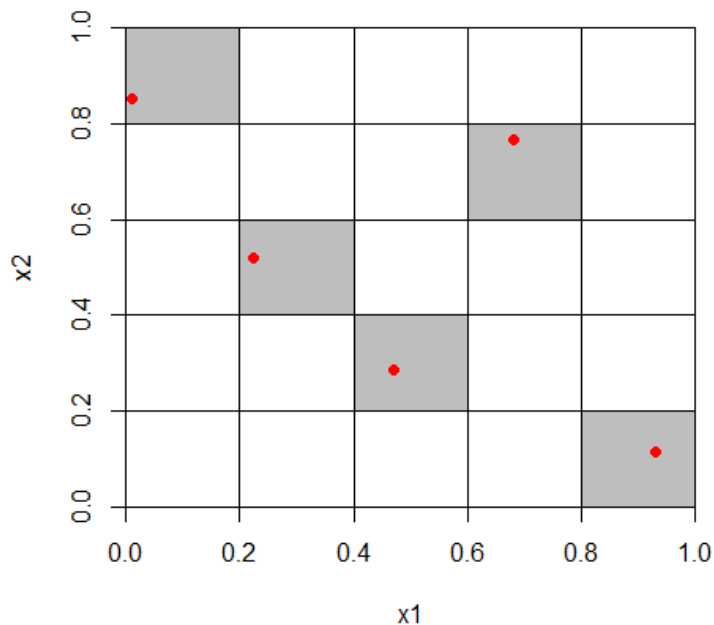
FEM input parameters	Symbol [unit]	Range
Pile diameter	D [m]	0.76 – 2.4
Pile slenderness	L/D [-]	10.0 – 60.0
Wall thickness ratio	D/t [-]	25.0 – 100.0
Soil relative density	D_r [%]	40.0 – 100.0
Dimensionless factor for elastic modulus	α [-]	3.0 – 9.0

Latin Hypercube Sampling - LHS

FEM: sampling with LHS

LHS is a sampling method enabling to better cover the domain of variations of the input variables, thanks to a **stratified sampling strategy**. The sampling procedure is based on dividing the range of each variable into several intervals of equal probability. The number of intervals equals the required sample dimension.

Example



Two linearly independent input variables both ranging from 0 to 1.

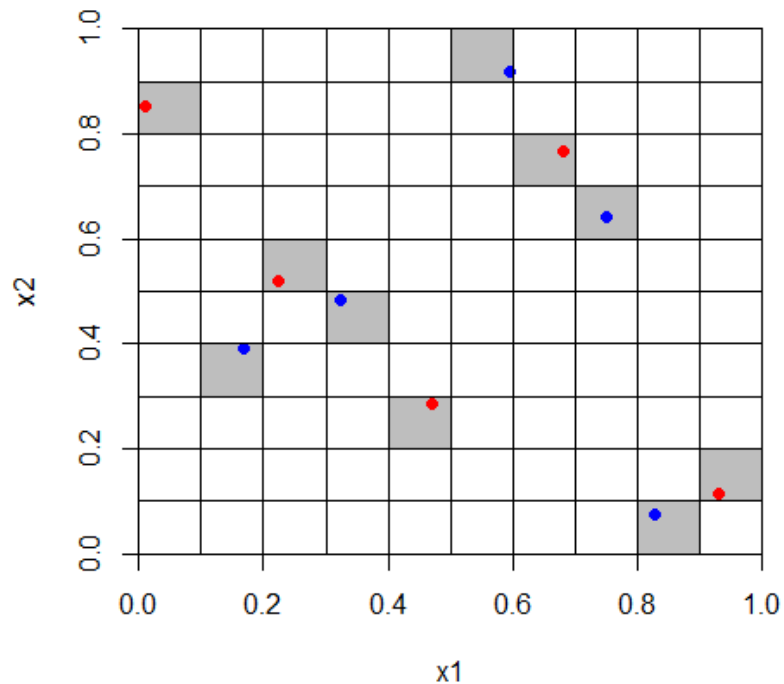
Sample size, $N = 5$

The Latin property of the hypercube requires that each of the 5 equal probability intervals (i.e. $1/5$) be filled (**i.e. each row and each column is filled with one point**).

Also notice that the exact location of the design point is randomly sampled within that cell using a uniform distribution for each marginal variable.

FEM: sampling with LHS

In case the sample size has to be enlarged, it can be done without losing its Latin Hypercube property.



Additional data, $N_{\text{add}} = 5 \rightarrow$ New Sample size, $N_{\text{new}} = 10$

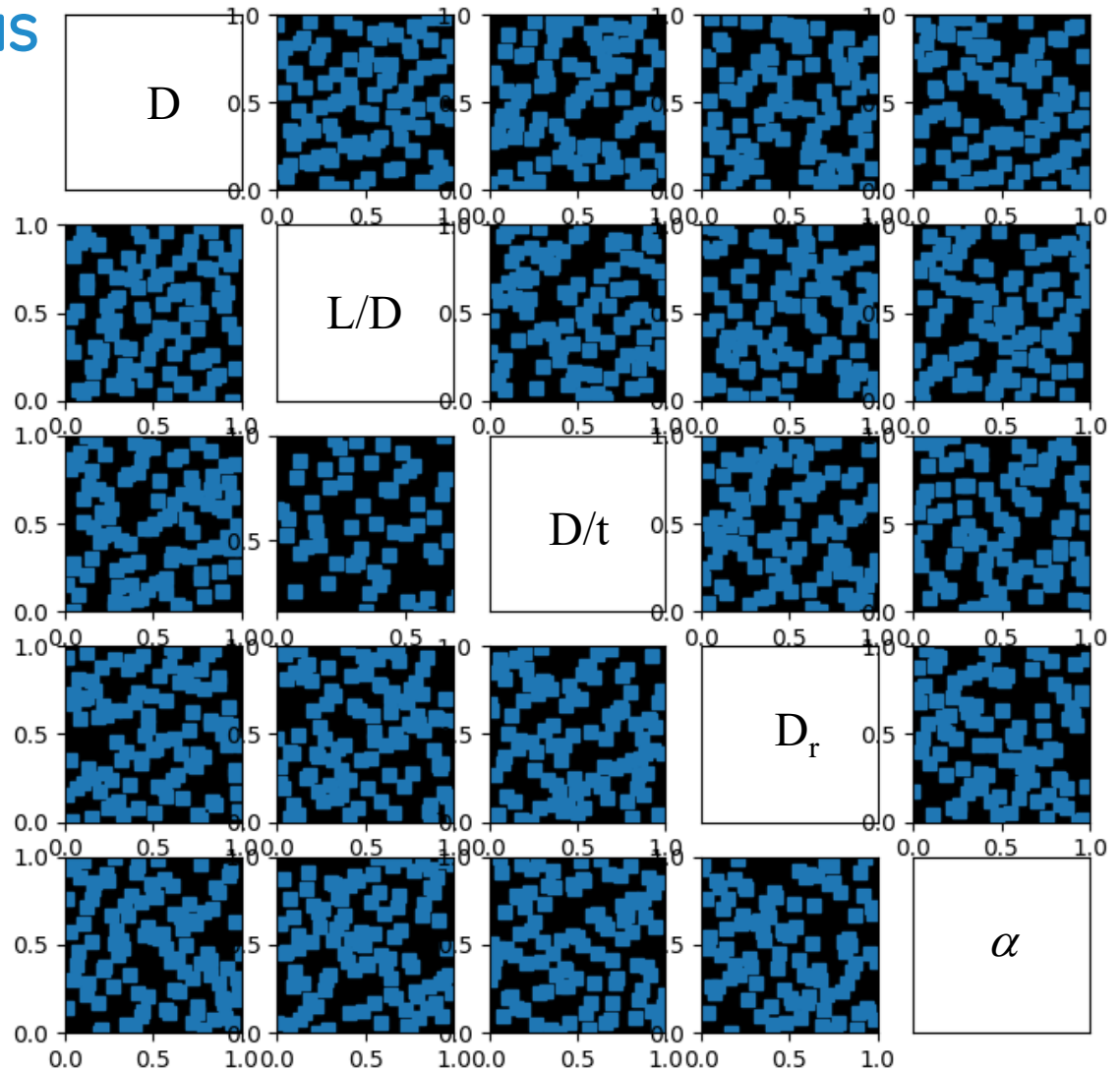
The additional data are added by re-dividing the original design into $N+N_{\text{add}}$ intervals (e.g. $5+5=10$) keeping the original design points exactly in the same position. It then randomly fills the empty row-column sets.

NOTE: the augmenting points do not necessarily form a Latin Hypercube themselves. The original design and augmenting points may form a Latin Hypercube, or there may be more than one point per row in the augmented design.

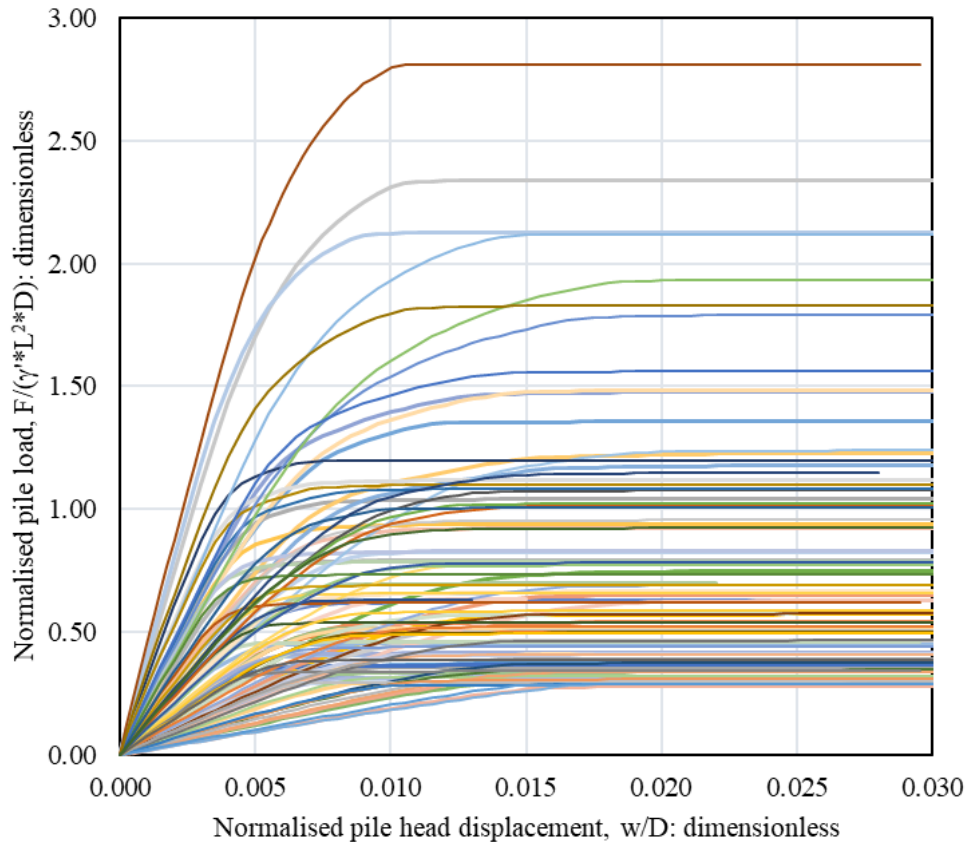
If the augmented points are equal to the number of original points, then a strictly uniform Latin hypercube is guaranteed.

FEM: sampling with LHS

N = 100



FEM: results



FEM input parameters	Symbol [unit]
Pile diameter	D [m]
Pile slenderness	L/D [-]
Wall thickness ratio	D/t [-]
Soil relative density	D_r [%]
Factor for elastic modulus	α [-]

FEM output	Symbol [unit]
Bearing capacity	Q [kN]
Initial stiffness	K [kN/m]



Metamodelling: the PCE

A **metamodel** or **surrogate** model is the model of a model, and **metamodeling** is the process of generating such metamodels. Metamodels are mathematical algorithms representing input and output relations. Metamodeling consists of learning the link between the two datasets.

If the prediction aim of the metamodel is to classify the observations in a set of finite labels, it is said to be a **classification** method. On the other hand, if the goal is to predict a continuous target variable, the metamodel is said to be a **regression** task.

Classification methods

Support Vector Classification
SVC

Regression methods

Polynomial Chaos Expansion
PCE



PCE: details

Input random vector of linearly independent parameters

$$\mathbf{X} = (X_1, \dots, X_n)^T$$

$$Y = \mathcal{M}(\mathbf{X})$$

Model response vector collecting Experimental or numerical observations

$$\mathbf{Y} = (Y_1, \dots, Y_n)^T$$

M may be a physical system or a computer code running a simulation, but **it is a black-box function**. The PCE is an approximation algorithm of this function, which **gathers all type of model response as the projection of the physical model in an orthonormal basis space**.

$$Y \approx \hat{M}(X) = \sum_{k \in K} \alpha_k \Psi_k(Z)$$

- $\Psi_k(\mathbf{Z})$ are multivariate polynomials orthonormal basis with respect to the PDF of Z ($f_{\mathbf{Z}}$)
- α_k are the corresponding coefficients

$\mathbf{Z} = T(\mathbf{X})$ T is an isoprobabilistic transform applied to the input variables



<https://openturns.github.io/openturns/latest/index.html>

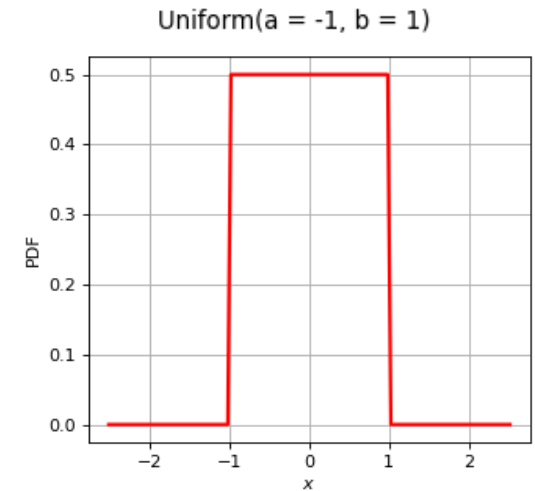


PCE: details

$$\mathbf{Z} = T(\mathbf{X})$$

Classical families of univariate orthonormal polynomials

Standard distribution	Polynomial
Normal $\mathcal{N}(\mu = 0, \sigma = 1)$	HermiteFactory
Uniform $\mathcal{U}(a = -1, b = 1)$	LegendreFactory
Gamma $\Gamma(k = k_a + 1, \lambda = 1, \gamma = 0)$	LaguerreFactory
Beta $\mathcal{B}(r = \beta + 1, t = \alpha + \beta + 2, a = -1, b = 1)$	JacobiFactory
Poisson $\mathcal{P}(\lambda)$	CharlierFactory
Binomial $\mathcal{B}(n, p)$	KrawtchoukFactory
NegativeBinomial $\mathcal{B}^-(r, p)$	MeixnerFactory



Orthonormal polynomial basis

Inner product for orthonormality property of the polynomial basis

$$\langle \psi_i, \psi_j \rangle = \int_D \psi_i(x) \psi_j(x) f_X(x) dx = \delta_{i,j}$$

PCE: details - Truncation strategy of the multivariate orthonormal basis

A strategy must be chosen for the selection of the different terms of the multivariate basis in which the response surface by functional chaos is expressed. The selected terms are regrouped in the finite subset K of \mathbb{N} .

There are three different strategies available:

- **FixedStrategy**,
- **SequentialStrategy**,
- **CleaningStrategy**.

@ Adaptive Strategy

https://openturns.github.io/openturns/latest/user_manual/response_surface/generated/openturns.AdaptiveStrategy.html#openturns.AdaptiveStrategy

PCE: details - Evaluation strategy of the coefficients, α_k

@ Projection Strategy

https://openturns.github.io/openturns/latest/user_manual/response_surface/generated/openturns.ProjectionStrategy.html#openturns.ProjectionStrategy

The vector $\alpha = (\alpha_k)_{k \in K}$ is equivalently defined by:

$$\alpha = \underset{\alpha \in \mathbb{R}^K}{\operatorname{argmin}} \mathbb{E} \left[\left(g \circ T^{-1}(\mathbf{Z}) - \sum_{k \in K} \alpha_k \Psi_k(\mathbf{Z}) \right)^2 \right] \quad \text{Least squares strategy} \quad (1)$$

and:

$$\alpha_k = \langle g \circ T^{-1}(\mathbf{Z}), \Psi_k(\mathbf{Z}) \rangle_{\mu} = \mathbb{E} [g \circ T^{-1}(\mathbf{Z}) \Psi_k(\mathbf{Z})] \quad \text{Integration strategy} \quad (2)$$

where $\mathbf{Z} = T(\mathbf{X})$ and the mean $\mathbb{E}[\cdot]$ is evaluated with respect to the measure μ .

PCE: details - looking through the PCE...

isoprobabilistic transform $\mathbf{Z} = T(\mathbf{X})$

FEM input parameters	Symbol [unit]	Range
Pile diameter	D [m]	0.76 – 2.4

ComposedDistribution(**Uniform(a = 0.76, b = 2.4)**, [...])

$$T(X) \equiv 2f_X(x) \cdot (x - E(X))$$

$$f_X(x) = \frac{1}{b - a}, \quad x \in [a; b]$$

$$E[X] = \frac{a + b}{2}$$

$$| y_0 = [x_0] \rightarrow [1.2195 \cdot (x_0 - 1.58)]$$



PCE: details – looking through the PCE...

[1, zero degree

1.73205 * x0, 1.73205 * x1, 1.73205 * x2, 1.73205 * x3, 1.73205 * x4, degree one

-1.11803 + 3.3541 * x0^2, [...] degree two

[...], 1.12741 - 40.5868 * x4^2 + 223.228 * x4^4 - 386.928 * x4^6 + 207.283 * x4^8] degree eight

```

0 : [ 0.774293 124.217 ]
1 : [ -0.0934781 -23.1485 ]
2 : [ -0.299315 -68.9418 ]
3 : [ -0.0487808 -0.00423974 ]
[...]
84 : [ -0.00532252 -0.895583 ]
85 : [ 0.00353601 0.88392 ]
86 : [ 0.00243645 0 ]

```

#87 (x2)
coefficients

α_k

#87

Legendre orthonormal
polynomial basis

Ψ_k





PCE: details – looking through the PCE...

0: zero degree

1.73205 * x0, 1.73205 * x1, 1.73205 * x2, 1.73205 * x3, 1.73205 * x4, degree one

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```

#87 (x2)
coefficients
 α_k

```

[0.774293, 124.217] + [-0.0934781, -23.1485] * (1.73205 * x0) + [-0.299315, -68.9418] * (1.73205 * x1) + [-0.0487808, -0.00423974] *
(1.73205 * x2) + [0.334187, 44.3097] * (1.73205 * x3) +
[...]
+ [-0.00532252, -0.895583] * (1.12741 - 40.5868 * x2^2 + 223.228 * x2^4 - 386.928 * x2^6 + 207.283 * x2^8) + [0.00353601, 0.88392] *
(1.12741 - 40.5868 * x3^2 + 223.228 * x3^4 - 386.928 * x3^6 + 207.283 * x3^8) + [0.00243645, 0] * (1.12741 - 40.5868 * x4^2 + 223.228 *
x4^4 - 386.928 * x4^6 + 207.283 * x4^8)

```

#PCE (x2)

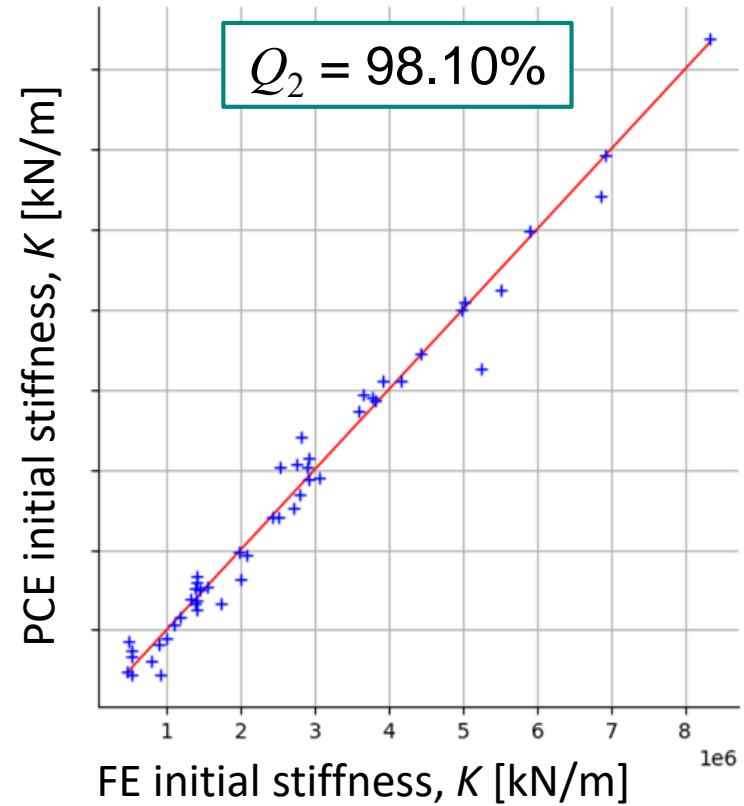
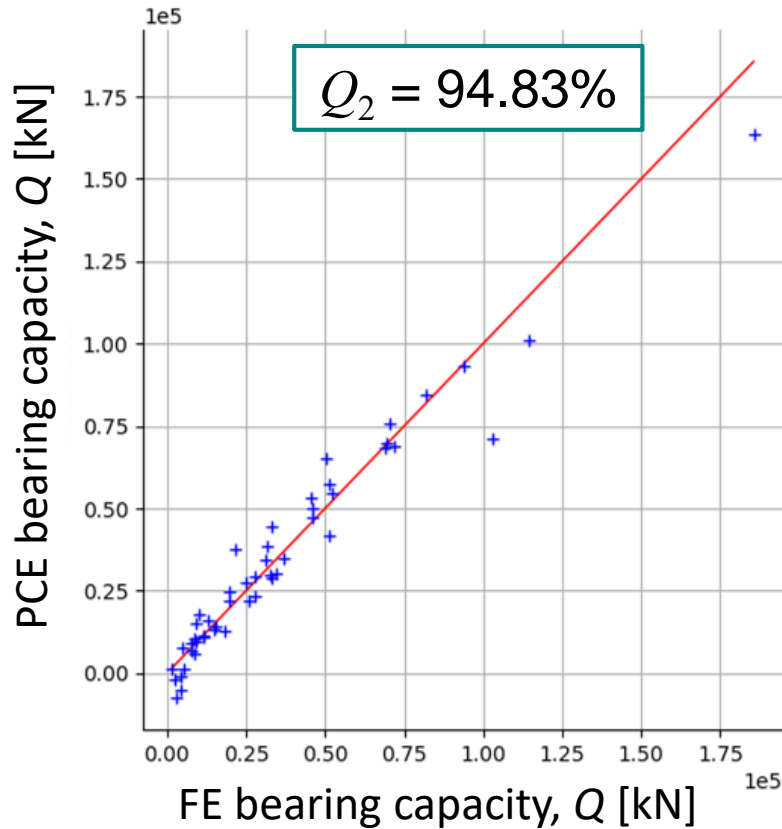
$$Y \approx \tilde{M}(X) = \sum_{k \in K} \alpha_k \Psi_k(Z)$$

#87
Legendre orthonormal
polynomial basis
 Ψ_k



PCE: results

PCE (N=100) Vs FEM (N=50)



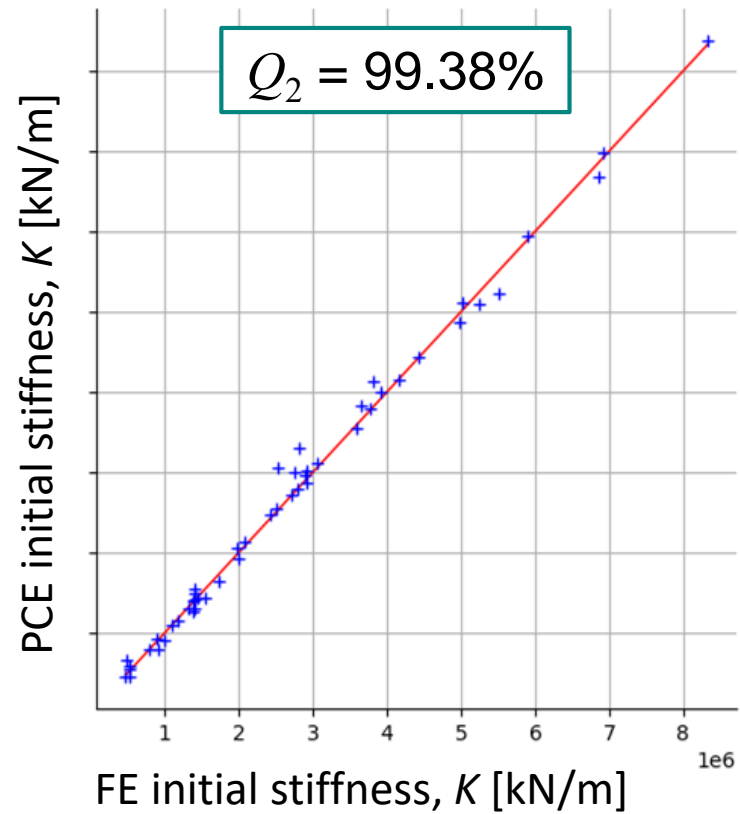
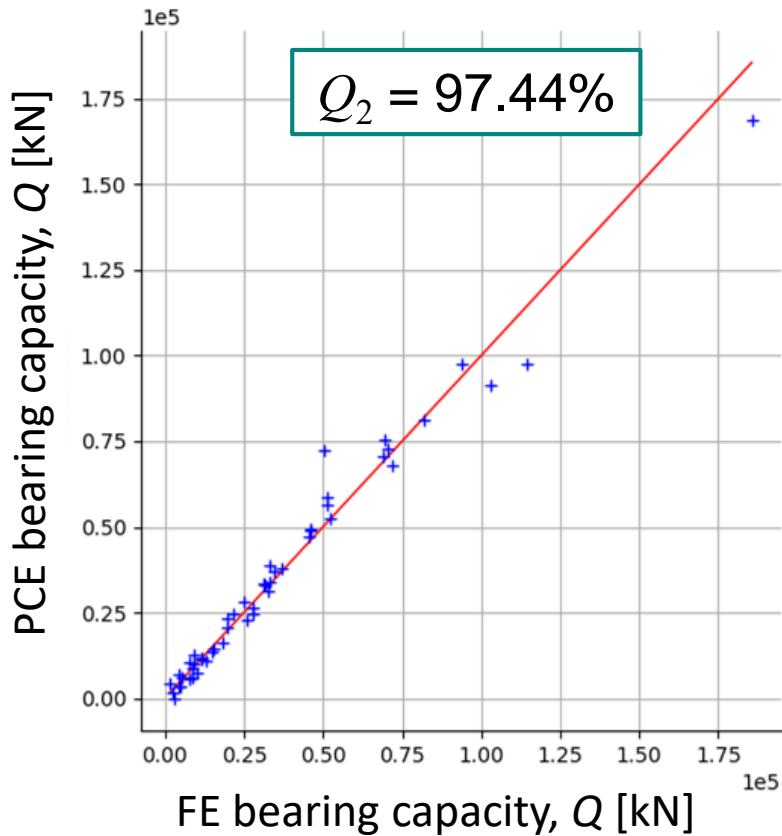
$$Q_2 = 1 - \frac{\sum_{l=1}^N (Y_l - \hat{f}(X_l))^2}{Var(Y)}$$

PCE: results

PCE (N=200) Vs FEM (N=50)

$Q_2 = 94.83\%$

$Q_2 = 98.10\%$

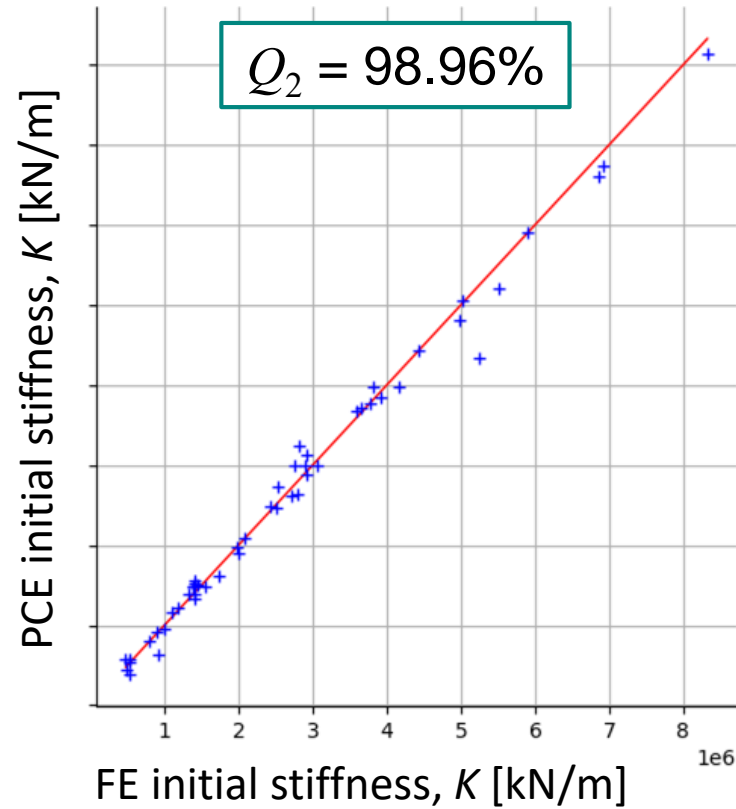
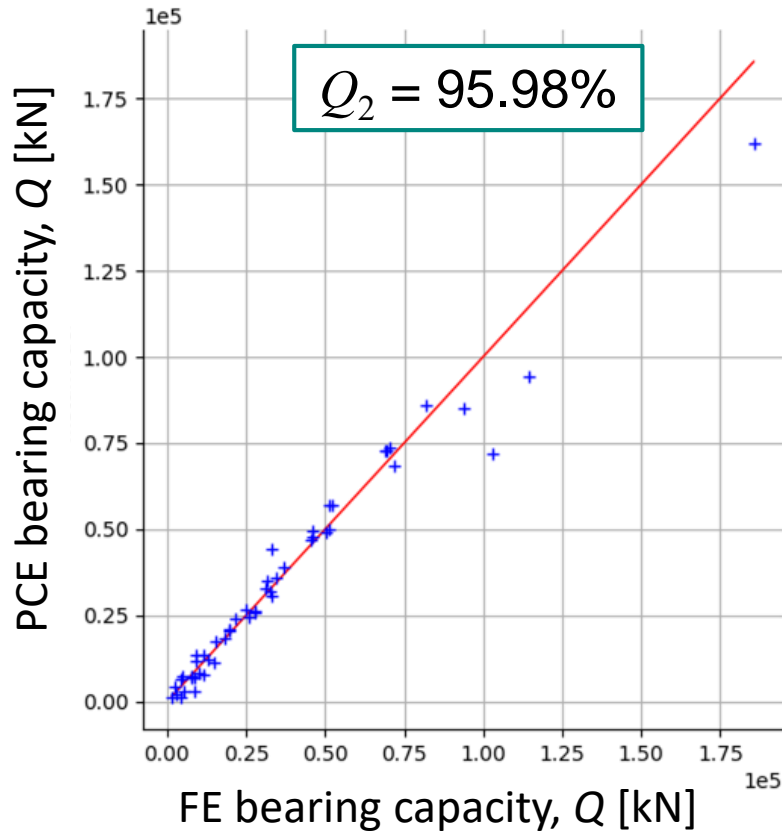


PCE: results

PCE_LOO (N=100) Vs FEM (N=50)

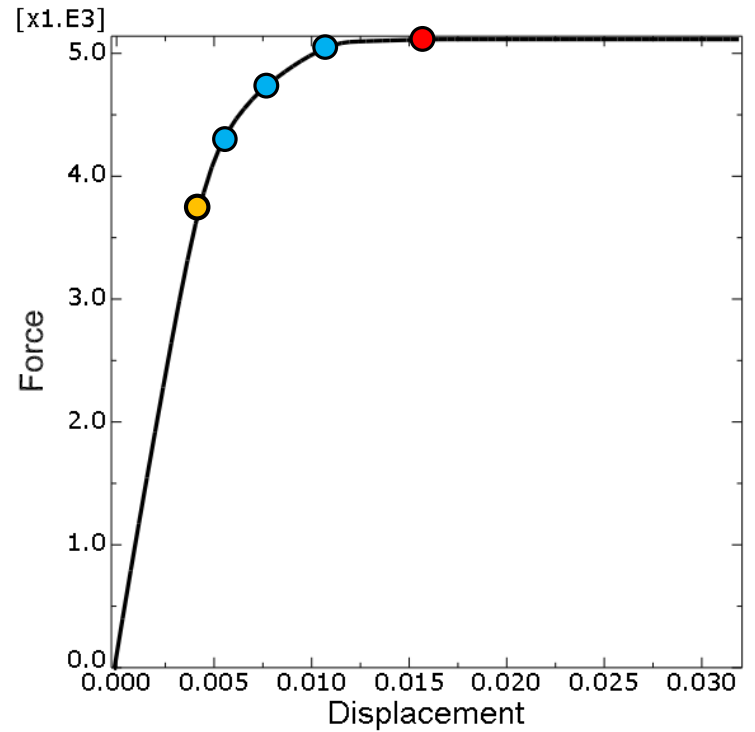
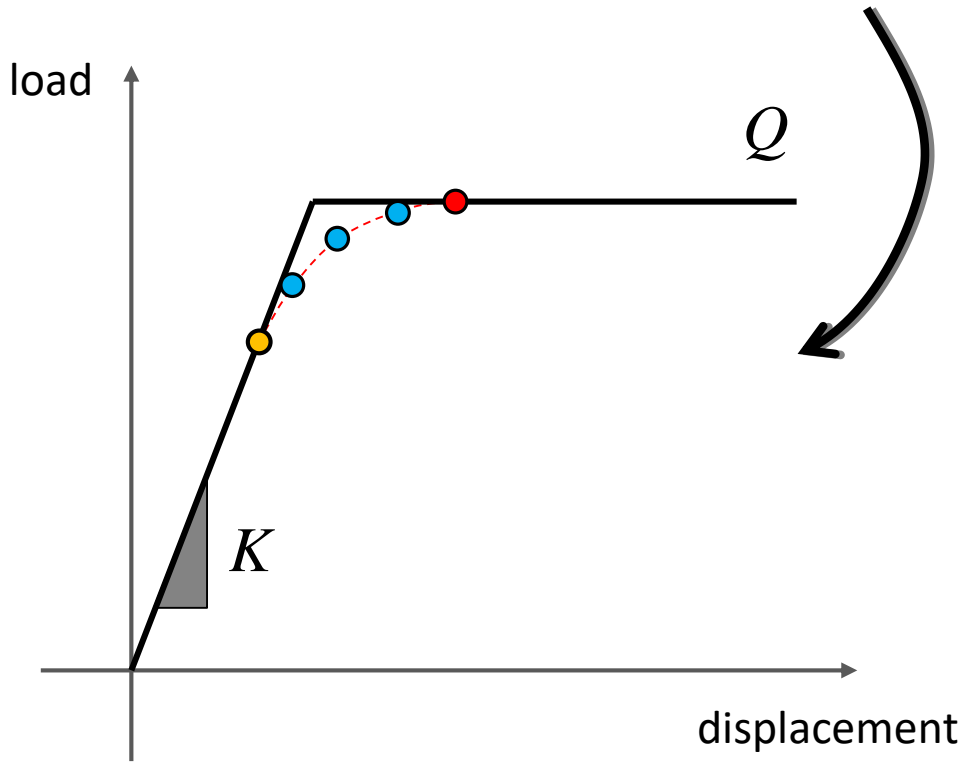
$Q_2 = 94.83\%$

$Q_2 = 98.10\%$



conclusions

input parameters	D [m]	L/D [-]	D/t [-]	D_r [%]	α [-]
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ALMA MATER STUDIORUM
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